Circuit breakers for direct current applications up to 380 V DC

Choosing and implementing protective devices





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Circuit breakers for DC applications up to 380 V DC Introduction

Direct current has been used for a long time, and in many fields. It offers major advantages, in particular simple storage with batteries. Moreover, direct-current Installations are now simpler, because they benefit from the development of power supplies with electronic converters and batteries.

- Telecommunication infrastructure:
- Electrical supply for industrial PLCs:
- □ PLCs and peripheral devices (24 or 48 V DC).
- Auxiliary uninterruptible direct current power supply:
- $\hfill\square$ relays or electronic protection units for MV cubicles,
- switchgear opening / closing coils and motors,
- □ LV control and monitoring relays,
- □ indicator lights,
- □ circuit-breaker or on/off switch motor drives,
- □ power contactor coils,
- □ communicating control/monitoring and supervision devices.





Circuit breakers for DC applications up to 380 V DC **Scope**

This application paper seeks to offer guidance in selecting the best protection and control components for a given DC system. It covers DC systems supplied by rectifier (AC/DC or DC/DC converter) and/or battery, isolated or connected to earth. The main voltages are 24 V DC, 48 V DC, 110 V DC, 220 V DC and 380 V DC.

Selection of devices in DC can be challenging due to the diversity of voltage levels and earthing system.

In this document we will consider the following systems:

п	TN		
Isolated from earth + and - conductors protected and disconnected	 - (or +) earthed + and - conductors protected and disconnected 	Midpoint earthed (not distributed) + and - conductors protected and disconnected	 - (or +) earthed + (or -) conductor only protected and disconnected
Load Load Load Load	Load	Load U/2 U/2 U/2 Load	Load B

Disconnection of one or two polarities in TN ?

IEC 60364 Electrical Installation Rules (Chapter 42) can be applied to protect and break only the polarity that is not earthed in TN, but both + & - conductors are "active" conductors, so we recommend disconnecting both polarities.

Positive or negative polarity earthed in TN ?

According to IEC 60479-1 upward current is twice as dangerous as downward current so for protection against electric shock it is recommended to earth the negative pole. (In some DC applications the positive polarity can be earthed for galvanic corrosion reason).

Circuit breakers for DC applications up to 380 V DC **Scope**

Circuit breaker selection

Selection of a circuit breaker depends essentially on the distribution-system parameters presented below which are used to determine the corresponding characteristics: (Page A4 of NSX DC catalog).

- Type of system determines the type of product and the number of poles connected in series for each polarity.
- Rated voltage determines the number of series poles taking part in current interruption.
- Nominal current determines the rated current of the circuit breaker.
- Maximum short-circuit current at the point of installation determines the breaking capacity.

Types of systems			
	Earthed systems		Isolated systems
	The source has one earthed polarity ⁽¹⁾	The source has an earthed mid-point	
Diagrams and various faults	· · · · ·		
Fault analysis (neglecting resist	Load or	Load U/2 U/2 U/2 U/2 Load	
Fault A	Maximum Isc at L	Maximum Isc at LI/2	No consequences
	 Only protected polarity concerned All poles of protected polarity must have breaking capacity > Isc max. at U 	 Only positive polarity concerned All poles of positive polarity must have breaking capacity ≥ lsc max. at U/2 	 The fault must be indicated by an IMD (insulation-monitoring device) and cleared (standard IEC/EN 60364)
Fault B	 Maximum Isc at U If only one polarity (the positive here) is protected, all poles of protected polarity must have breaking capacity ≥ Isc max. at U If both polarities are protected, to enable disconnection, all poles of the two polarities must have breaking capacity ≥ Isc max. at U 	 Maximum Isc at U Both polarities are concerned All poles of the two polarities must have breaking capacity Isc max. at U 	 Maximum Isc at U Both polarities are concerned All poles of the two polarities must have breaking capacity Isc max. at U
Fault C	No consequences	 Same as fault A All poles of the Negative polarity must have breaking capacity ≥ lsc max. at U/2 	Same as fault A with the same obligations
Double fault A and D or C and E	Double fault not possible, system trips on first fault	Double fault not possible, system trips on first fault	 Maximum Isc at U Only positive polarity (cases A and D) or negative polarity (C and E) concerned All poles of each polarity must have breaking capacity ≥ Isc max. at U
Most unfavorable cases			
	Fault A and fault B (if only one polarity is protected)	Fault B	Double fault A and D or C and E

Switch-disconnector selection

For a TN system switch-disconnectors have to break load current only, so the above rules are simplified:

If the negative and positive polarities are disconnected, the switch-disconnector must be able to break the load current with the two poles (or 2×2 poles in series) at system voltage, If the negative OR positive polarity only is disconnected, the switch-disconnector must be able to break the load current with one pole (or 1×2 poles in series) at system voltage.

For an IT system, switch-disconnectors have to break load current, but the risk of opening in a double fault situation cannot be ruled out, so we recommend to selecting a switch-disconnector for IT as circuit breaker if there is no action at the first fault detection.

If switch-disconnectors are used for the isolation function, the load current breaking constraint could be eliminated, but special marking and interlock would have to be implemented to prevent operation under load.

Environment		Voltage specifica	ations
		AC	DC
Dry environment Zman = 2000 Ohms	Uf = Z x If	50 V	120 V
Vet environment Zman = 1000 Ohms	Uf = Z x If	25 V	60 V





Protection against electric shocks

In 24 or 48 V DC applications, the "extra-low-voltage" (SELV or PELV) is usually the protective measure for protection of persons against electrical shocks in case of fault. The table on the left shows the voltage limits according to the IEC 60479-2 standard. In that case, the circuit breakers are required only for circuit protection against over-currents (overload, short-circuit and earth fault).

The voltage level is not enough to ensure compliance with SELV or PELV requirements: the source and circuits must also comply with IEC 60364-4-41-414 (isolation/separation from higher voltage system).

If "automatic disconnection of the supply" is the protective measure selected, then the circuit breaker tripping time for a minimum earth fault current shall be checked according to table 41.1 of IEC 60364 -4-41.

In IT an insulation monitoring system is mandatory. See "Chapter E page 24".

Selection of circuit breaker (Table A.1 page 8)

Range, rating and number of poles

"Table A.1" shows our recommended solution according to the earthing system and current rating for short-circuit currents up to 10 kA (alternative solutions are also proposed for higher short-circuit currents up to 36 kA).

Tripping curves

The tripping curves for C60HDC/iC60/C120/NG125 ranges shall be selected according to the load (inrush current), see "Appendix A page 27". In some applications polarized circuit breakers (C60H-DC) cannot be used, see "Appendix B page 27".

Discrimination

The 230/400 V AC discrimination table cannot be used in DC. See example below. The tables for DC are available in complementary technical information 2017.

Selection of switch-disconnector (Table A.2 page 10)

Range, rating and number of poles

"Table A.2" shows our recommended solution according to the earthing system and current rating.

Coordination with circuit breaker

All switches must be protected by an over-current protection device located upstream.

The switch-disconnector proposed in "Table A.2 page 10" are fully coordinated with the circuit breakers of "Table A.1 page 8" up to 10 kA.

Example of 48 V DC system with 3 levels of circuit breaker and total discrimination



7

Table A.1: circuit breaker selection for 24/48 V DC according to earthing system



(1) IM10 or IM20 or IM400 see selection criteria "Insulation monitoring system for DC application", page 24

8

А

Circuit breakers for DC applications up to 380 V DC 24/48 V DC application

Complement for short-circuit currents higher than 10 kA



(1) NG125H (80 A Max) up to 25 kA

IMD see Table A.1

24/48 V DC Presumed short-circuit current Isc ≤ 36 kA					
Earthing system	IT	TN			
	Isolated from earth + and - conductors protected and disconnected	- (or +) earthed + and - conductors protected and disconnected	Midpoint earthed (not distributed) + and - conductors protected and disconnected	- (or +) earthed + (or -) conductor only protected and disconnected	
	Load to the set of the		Load B		
CB rating					
≤ 80 A					
	NG125L2P			NG125H 1P	
I > 80 A		BID 07222.05 eps	PB107529-35. eps		
	Compact NSX DC F (see Table	e B.1 page 12) 110 V DC applic	ation		

IMD see Table A.1

Table A.2: switch-disconnector selection for 24/48 V DC according to earthing system



(1) Current carrying capacity of Compact INS Switch-disconnector with parallel connection of poles:

- 2 poles used: $Ith = 1.6 \times In$,

- 3 poles used: Ith = 2.25 x In.

Example: an INS80 with 2 poles in parallel can be used up to 80 x 1.6 = 128 A,

INS80 with 3 poles in parallel can be used up to 180 A.

(2) Prospective short-circuit current of switch-disconnector with related circuit breaker:

	iSW	INS 40/63/80	INS 100/125/160
	le ≤ 63 A	le ≤ 80 A	le ≤ 160 A
iC60N/H/L	10 kA	10/15/20 kA	10/15/20 kA
C60H-DC (In ≤ 63 A)	10 kA	20 kA	20 kA
C120N/H (In ≤ 125 A)	-	10/15 kA	10/15 kA
NG125N/H/L	-	20/25/36 kA	20/25/36 kA
NSX160 (In ≤ 160 A)	-	-	36 kA

The circuit breaker's rating or "Ir" setting shall be less than or equal to the rated current of the switch-disconnector.

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Protection against electric shocks

In 110 V DC applications, "extra-low-voltage" (SELV or PELV) is usually the protective measure for protection of persons against electrical shocks in case of fault. The table below shows the voltage limits according to the IEC 60479-2 standard. In that case, the circuit breakers are required only for circuit protection against over-current (overload, short-circuit and earth fault).

The voltage level is not enough to ensure compliance with SELV or PELV requirements: the source and circuits must also comply with IEC 60364-4-41-414 (isolation/separation from higher voltage system).

If "automatic disconnection of the supply" is the protective measure selected, then the circuit-breaker tripping time for a minimum earth fault current shall be checked according to table 41.1 of IEC 60364 -4-41.

In IT, an insulation monitoring system is mandatory. See "Chapter E page 24".

Environment		Voltage specifications	
		AC	DC
Dry environment Zman = 2000 Ohms	Uf = Z x If	50 V	120 V
Wet environment Zman = 1000 Ohms	Uf = Z x lf	25 V	60 V

Selection of circuit breaker (Table B.1 page 12)

Range, rating and number of poles

"Table B.1" shows our recommended solution according to the earthing system and current rating for short-circuit currents up to 10 kA. (alternative solutions are also proposed for higher short-circuit currents up to 36 kA).

Tripping curves

The tripping curves for C60H-DC/iC60/C120/NG125 ranges shall be selected according to the load (inrush current), see "Appendix A page 27" and requirements for protection against electric shock, where applicable (see above). In some applications polarized circuit breakers (C60H-DC) cannot be used, see "Appendix B page 27".

Discrimination

The 230/400 V AC discrimination table cannot be used in DC. The tables for DC are available inside complementary technical information 2017. See example below.

Selection of switch-disconnector (Table B.2 page 14)

Range, rating and number of poles

Table B.2 shows our recommended solution according to the earthing system and current rating.

Coordination with circuit breaker

All switches must be protected by an over-current protection device located upstream.

The switch-disconnectors proposed in "Table B.2 page 14" are fully coordinated with circuit breakers of "Table B.1 page 12" up to 10 kA.

Example of 110 V DC system with 3 levels of circuit breaker and total discrimination



В

Table B.1: circuit breaker selection for 110 V DC according to earthing system



В

Circuit breakers for DC applications up to 380 V DC 110 V DC application

Complement for short-circuit currents higher than 10 kA



IMD see Table B.1

110 V DC Presumed short-circuit current lsc ≤ 36 kA					
Earthing system	IT	TN			
	Isolated from earth + and - conductors protected and disconnected	 (or +) earthed + and - conductors protected and disconnected 	Midpoint earthed (not distributed) + and - conductors protected and disconnected	- (or +) earthed + (or -) conductor only protected and disconnected	
			Load Hereit		
CB rating					
≤ 80 A				Desta 19, 28, 30, 30, 28, 30, 30, 30, 30, 30, 30, 30, 30, 30, 30	
	NG125L2P			NG125H 1P	
I > 80 A		PB107225.6ps	PB107225-36 eps		
	Compact NSX DC F (see Table B.1 page 12) (starting with 80/100/125 A ratings)				

IMD see Table B.1

Table B.2: switch-disconnector selection for 110 V DC according to earthing system



Table B.2 (cont.): switch-disconnector selection for 110 V DC according to earthing system

110 V DC Presumed short-circuit current lsc ≤ 10 kA ⁽²⁾				
Earthing system	ІТ	TN		
	Isolated from earth + and - conductors protected and disconnected	- (or +) earthed + and - conductors protected and disconnected	Midpoint earthed (not distributed) + and - conductors protected and disconnected	- (or +) earthed + (or -) conductor only protected and disconnected
SW rating				
le = 160 A - 250 A	PB11140-40.eps	PB111436-40.eps	BBIII 406 40 FBI	BII1406-40-698
	INS250 4P (2x2P in serie)	INS250 3P (1P+2P in serie)	INS160 4P ⁽¹⁾ (2x2P parallel)	INS160 4P ⁽¹⁾ (2x2P parallel in serie)
250 - 400 A	PBIII400-00 ops	PBIII438-40 ops	PBIII400-00 ops	PHI4040 es
			↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓	, , , , , , , , , , , , , , , , , , ,
	INS320/400 4P	INS320/400 3P	INS250 4P ⁽¹⁾ (2x2P parallel)	INS250 4P ⁽¹⁾
	(ZXZP IN Serie)	(1P+2P in serie)		(ZXZP parallel in serie)

(1) Current carrying capacity of Compact INS Switch-disconnector with parallel connection of poles:
2 poles used: Ith = 1.6 x In,
3 poles used: Ith = 2.25 x In.

Example: an INS80 with 2 poles in parallel can be used up to 80 x 1.6 = 128 A,

INS80 with 3 poles in parallel can be used up to 180 A.

(2) Prospective short-circuit current of switch-disconnector with related circuit breaker:

	iSW	INS 40/63/80	INS 100/125/160
	le ≤ 63 A	le ≤ 80 A	le ≤ 160 A
iC60N/H/L	10 kA	10/15/20 kA	10/15/20 kA
C60H-DC (In ≤ 63 A)	10 kA	20 kA	20 kA
C120N/H (In ≤ 125 A)	-	10/15 kA	10/15 kA
NG125N/H/L	-	20/25/36 kA	20/25/36 kA
NSX160 (In ≤ 160 A)	-	-	36 kA

The circuit breaker's rating or "Ir" setting shall be less than or equal to the rated current of the switch-disconnector.

В

Protection against electric shocks

Except for TN with Midpoint Earthed where SELV/PELV is still an option, the protective measure is usually "automatic disconnection of the supply" for this voltage level. The circuit-breaker tripping time for a minimum earth fault current shall be checked according to Table 41.1 of IEC 60364 -4-41.

In IT, an insulation monitoring system is mandatory. See "Chapter E page 24".

Selection of circuit breaker (Table C.1 page 17)

Range, rating and number of poles

"Table C.1" shows our recommended solution according to the earthing system and current rating for short-circuit currents up to 10 kA. (alternative solutions are also proposed for higher short-circuit currents up to 36 kA).

Tripping curves

The tripping curves for C60H-DC/iC60/C120/NG125 ranges shall be selected according to the load (inrush current), see "Appendix A page 27" and requirements for protection against electric shock, where applicable (see above). In some applications, polarized circuit breakers (C60H-DC) cannot be used, see "Appendix B page 27".

Discrimination

The 230/400 V AC discrimination table cannot be used in DC. The tables for DC are available in complementary technical information 2017. See example below.

Selection of switch-disconnector (Table C.2 page 19)

Range, rating and number of poles

"Table C.2" shows our recommended solution according to the earthing system and current rating.

Coordination with circuit breaker

All switches must be protected by over-current protection device located upstream. The switch-disconnectors proposed in "Table C.2 page 19" are fully coordinated with the circuit breakers of "Table C.1 page 17".

Example of 220 V DC system with 3 levels of circuit breaker and total discrimination



Table C.1: circuit breaker selection for 220 V DC according to earthing system



See Compact NSX, Compact INS/INV, Masterpact NW DC- DCPV, catalog page B-7 for detail tripping characteristics with parallel connections.
 IM10 or IM20 or IM400 see selection criteria "Insulation monitoring system for DC application", page 24

С

Complement for short-circuit currents higher than 10 kA



(1) NG125H up to 25 kA

IMD see Table C.1

220 V DC Pres	220 V DC Presumed short-circuit current lsc ≤ 36 kA					
Earthing system	IT	TN				
	Load Healing					
CB rating	1					
In ≤ 63 A		06439_SE-30 eps	sde or: 30, 30, 30, 30, 30, 30, 30, 30, 30, 30,	Star 25600PA		
	Load	Load				
	NG125L4P (2x2P serie)	NG125L 3P (1P+2P serie)	NG125L2P	NG125L2P		
I≥80A		PB10722.35.app	PB107526-35.ept			
	Compact NSX DC F as for 10 kA (see Table C.1 page 17) (starting with 80/100/125 A ratings)					

IMD see Table C.1

Table C.2: switch-disconnector selection for 220 V DC according to earthing system

220 V DC Pres	umed short-circuit curr	ent Isc ≤ 10 kA ⁽¹⁾		
Earthing system	іт	ТN		
	Isolated from earth + and - conductors protected and disconnected	 (or +) earthed + and - conductors protected and disconnected 	Midpoint earthed (not distributed) + and - conductors protected and disconnected	- (or +) earthed + (or -) conductor only protected and disconnected
SW rating				
le ≤ 63 A				
	NSX100NA 3P (2P used)	iSW 4P (1P+3P serie)	iSW 4P (2x2P serie)	iSW 4P (4P serie)
le ≤ 80 A		PB111402-40 eps	PB111402 40 opt	BH11402.40 GPS
		Load		Logd 4P (4P sorio)
le = 100 - 250 A		1N340/80 4F (1F+3F)		
	or vesicolad	BBH140640.6		BBIII10849 eps
	NSX100 - 250NA 3P	INS100 - 160 - 250 4P	INS100 - 160 - 250 4P	INS100 - 160 - 250 4P
le = 400 A - 630 A	(2P used)	(1P+3P serie)	(2x2P serie)	(4P serie)
	used)	(1P+3P serie)	1113400 - 030 4P (2X2P Selle)	11N3400 - 030 47 (47 Serie)
(4) D (1) (1) (1)				

(1) Prospective short-circuit current of switch-disconnector with related circuit breaker:

	iSW	INS				NSX		
	(63A)	40/63/80	100/125/160	250	320/630	100 - 160NA	250NA	400 - 630NA
iC60N/H/L	10 kA	10/15/20 kA						
C60H-DC (In ≤ 63 A)	10 kA	20 kA	20 kA	20 kA	20 kA	20 kA	20 kA	20 kA
C120N/H (In ≤ 125 Å)	-	10/15 kA						
NG125N/H/L	-	20/25/36 kA						
NSX100/160 (In ≤ 160 A)	-	-	36 kA					
NSX250	-	-	-	36 kA	36 kA	-	36 kA	36 kA
NSX400-630	-	-	-	-	36 kA	-	-	36 kA

The circuit breaker's rating or "Ir" setting shall be less than or equal to the rated current of the switch-disconnector.

Protection against electric shocks

The protective measure is usually "automatic disconnection of the supply" for this voltage. The circuit-breaker tripping time for a minimum earth fault current shall be checked according to Table 41.1 of IEC 60364 -4-41.

In IT, an insulation monitoring system is mandatory. See "Chapter E page 24".

Selection of circuit breaker (Table D.1 page 21)

Circuit breakers in addition to automatic disconnection of the supply ensure conductor protection against overloads and short-circuits. Their tripping characteristics shall be selected according to the conductors protected. Range, rating and number of poles

"Table D.1" shows our recommended solution according to the earthing system and current rating for short-circuit currents up to 10 kA (alternative solutions are also proposed for higher short-circuit currents up to 36 kA).

In some applications, polarized circuit breakers (C60H-DC) cannot be used, see "Appendix B page 27".

Tripping curves

The tripping curves for C60H-DC/iC60/C120/NG125 ranges shall be selected according to the load (inrush current), see "Appendix A page 27" and requirements for protection against electric shock, where applicable (see above). Discrimination

The 230/400 V AC discrimination table cannot be used in DC. The tables for DC are available in complementary technical information 2017. See example below.

Selection of switch-disconnector (Table D.2 page 23)

Range, rating and number of poles

"Table D.2" shows our recommended solution according to the earthing system and current rating.

Coordination with circuit breaker

All switches must be protected by an over-current protection device located upstream.

The switch-disconnectors proposed in "Table D.2 page 23" are fully coordinated with the circuit breakers of "Table D.1 page 21".

Example of 380 V DC system with 3 levels of circuit breaker and total discrimination



Table D.1: circuit breaker selection for 380 V DC according to earthing system

380 V DC Presumed short-circuit current lsc ≤ 10 kA						
Earthing	IT	TN				
system	Isolated from earth + and - conductors protected and disconnected	- (or +) earthed + and - conductors protected and disconnected	Midpoint earthed (not distributed) + and - conductors protected and disconnected	- (or +) earthed + (or -) conductor only protected and disconnected		
	Ster weeking					
CB rating	Ø		0	0 L 0		
IN ≤ 63 A	068335 EE - 00 eb					
	NG125N 4P (2x2P serie)	NG125N 4P (1P+3P serie)	C60H-DC 2P	C60H-DC 2P		
80 - 125 A			SOUL-DO T			
			- + - %			
	NG125N 4P (2x2P serie)	NG125N or C120N 4P	C120N 4P (2x2P serie)	C120N 3P (serie)		
125 - 160 A						
	NSX160F DC 4P (2x2P serie)	NSX160F DC 3P (1P+2P serie)	NSX160F DC 2P	NSX160F DC 2P (serie)		
200 - 630 A	Development		BBI13669 eps	DB400657 eps		
	PPI 07531-40.eps	PB10722736 aps	PB1072736.aps	sda at 7227 ta ap		
	NSX250/400/630F DC 4P	NSX250/400/630F DC 3P	NSX250/400/630F DC 3P	NSX250/400/630F DC 3P		
IMD	(2X2P serie)	(2P used)	(2P used)	(2P serie used)		

(1) IM10 or IM20 or IM400 see selection criteria "Insulation monitoring system for DC application", page 24

Complement for short-circuit currents higher than 10 kA



Table D.2: switch-disconnector selection for 380 V DC according to earthing system



36 kA

36 kA

The circuit breaker's "Ir" setting shall be less than or equal to the rated current of the switch-disconnector.

36 kA

NSX250

NSX400-630

Circuit breakers for DC applications up to 380 V DC **Insulation monitoring system for DC application**

Insulation monitoring is required whenever the DC installation is ungrounded.

Ungrounded DC applications

Ungrounded earthing is selected when continuity of service is critical on the application. Indeed, with ungrounded networks, the occurrence of an insulation fault does not require the trip of protections.

DC ungrounded applications include high availability applications such as :

- Nuclear power generating stations
- Other power generating stations
- Oil and Gas power distribution stations
- Other DC control systems
- Telecom
- Control command systems.

Note: Photovoltaic fields are other examples of ungrounded DC application, but are out of the scope of this document.

Selection of the Insulation Monitor for DC applications

In order to be compatible with the monitoring of ungrounded DC installations, the Insulation Monitor must not operate by the injection of a DC component on the network. Instead, the IMD should inject an alternative signal on the network. Considering the Vigilohm range; the IM9 is not suited for DC network monitoring. Instead the IM10, IM20 and IM400 will be selected.

	PB100372-35 cps	PB106374-35.eps	PB111226 40 eps
Maximum voltage	IM10 345 V DC	IM20 345 V DC	IM400 and IM400C 480 V DC
Leakage capacitance	40 µF	150 µF	2000 µF
Fault location device	No	No	XD301/312
Communication	No	Yes	Yes

The selection of IMD depends on criterias such as:

Size of the network and value of leakage capacitance

Disturbing loads on the network

- Need for automatic fault locators
- Need for Modbus communication

The environment: IM400C (coated version of IM400) can be selected when environmental conditions are harsh (humidity, important variation of temperature, salty atmosphere...).

As an option, **Insulation Fault Locators** can be installed in addition to the Insulation Monitor. The locators facilitate OPEX reduction by designating automatically the faulty feeder, keeping the continuity of service on the installation. If Insulation Fault Locators are needed, the recommendation is to use as the IMD the

IM400 together with XD3xx locators.

Circuit breakers for DC applications up to 380 V DC Insulation monitoring system for DC application

Examples of architecture

 $\mathsf{Example}$ of 380 V DC ungrounded network with Insulation Monitor and Fault Locators.



The Insulation Fault Locator detects the injected current from the IM400 through its toroid. The IM400 injects a low frequency component on the network (2.5 Hz) which allows measuring the network insulation, and locating the insulation fault. XD312 type of locator is suited for the automatic location of low impedance faults (typically less than 1 kOhm).

Installation of the IMD- Points of Attention

Connection of the injection

IMD injection is only connected on one of the polarity on the network. Whenever the network is including loads or battery, the injection signal of IMD will be able to flow in both polarities. As a consequence an insulation fault between any of the polarity and the ground will be properly detected.

Note: If there are no load and no battery on the installation, the injection signal of IMD only flows through the polarity it is connected to. An insulation fault between the other polarity and ground may not be detected. If this configuration was to happen, a system has to be implemented to connect for a few minutes the injection of IMD on one polarity, then next few minutes on the other polarity etc.

When available, it is suggested to connect the injection of IMD in the central point of the battery.

If this is not possible, then injection is connected to one of the polarities; and this creates an unbalance between the two phase voltages.

Blocking diodes

IMDs measuring current has the ability to go through blocking diodes, back and forward, as long as these diodes are polarized by the load current (high current). Every part of the DC auxiliary power system that is flown by load current is therefore monitored by the IMD.



Vigilohm IM400

Circuit breakers for DC applications up to 380 V DC **WWW.schne** To know more about Schneider Electric's DC offer

In addition to distribution for critical services as described in this guide, DC is also used in two other main applications: battery protection in UPS and storage systems and photovoltaic applications. Schneider Electric offers a comprehensive DC range for these three applications.





Compact NSX, Compact INS/INV, Masterpact NW, DC-DCPV catalog



Safe and reliable photovoltaic generation EDCED112005EN



Miniature circuit breakers for 24/48 V direct current applications **CA908032E**



Vigilohm catalog **PLSED310020EN**

Circuit breakers for DC applications up to 380 V DC Appendix



Example: iC60, B, C, D curves, ratings from 6 A to 63 A.

Batteries with rectifier/charger.

Appendix A: tripping curve for MCB

Choosing the curve

The magnetic tripping threshold must be:

- Higher than the inrush currents due to loads (motors, capacitors, etc.)
- Lower than the short-circuit current at the installation point, which depends on:
- □ the short-circuit power of the source (indicated by the manufacturer),
- □ the impedance of the supply line.

In direct current:

The short-circuit power of the sources is generally low: batteries, photovoltaic panels, generators, electronic converters, etc

The loads generate lower inrush currents than in alternating current (e.g. motor start-up: 2 to 4 times the rated current)

The magnetic threshold of Acti 9 circuit breakers (relative to the rated current) is higher than in alternating current.

Circuit breaker	iC60 / C120 / NG125				C60H-DC	
Curve	Z	В	С	D	С	
Magnetic tripping threshold	3.45 In	4.57 In	914 In	1420 In	710 ln	

Appendix B: polarized circuit breaker

For a battery application, the current can have 2 flows (battery to load or rectifier to battery).

The polarized circuit breaker or polarized switch-disconnector cannot be used.

Polarized circuit breaker	Non-polarized circuit breaker
C60H-DC	iC60N/H/L
	C120N/H
	NG125N/H/L
	NSX100-160DC F/N/M 1P - 2P
	NSX250DC F/S
	NSX400-630DC F/S

All Schneider Electric switch-disconnectors described in this technical guide are non-polarized.

Circuit breakers for DC applications up to 380 V DC Appendix



Appendix C: pole connection

Series connection

Series connection of the poles, by dividing the voltage per pole, optimizes the circuit breaking performance for high-voltage networks.

Series connection of the poles of a circuit breaker used in direct current therefore makes it possible to:

- Divide the network voltage by the number of poles
- Have the rated current for each pole
- Have the circuit breaker's breaking capacity for all the poles.

Direction of cabling and cable length

In the case of series connection, the direction of cabling has a major impact on the product's performance.

Usually the first product cabling method 1

will be used. For special applications where there is only a single possible current direction, the second cabling method (2) is preferable, especially for electrical endurance properties.

Subsequently the cable cross section and length combination should be optimized, depending on the loads. Generally, a greater length and cross section improves performance.

Rating (In)	Cross section (mm ²)	Min. shunt length (mm)
≤63A	≤16	500
	25	200
	35	100
≤ 125 A	35	300
	50	200

Note: this table gives the minimum cable (shunt) lengths optimizing the equipment's performance according to the cable cross sections.

Clarification concerning voltage drops

Importance of allowing for voltage drops

Voltage drops are an issue that must be taken into account especially in direct current distribution due to:

- The common use of very low voltage (24, 48 or sometimes 12 V):
- □ for a given resistance and current in a circuit, increasing relative voltage drops increase as the voltage is lowered,
- natural voltage drop of batteries in power reserve mode, as they are discharged,
 criticality of associated applications, often requiring a high level of security and continuity of service.

Cause of voltage drops

Voltage drops are caused by the sum of the resistances in series in the circuit:

- Internal resistance (r) of the source
- Resistance of connecting cables
- Internal resistance of control and protection switchgear, often significant for circuit breakers of low rating (a few amperes) powered at very low voltage
- Generally expressed in mΩ
- Which, if there is no direct data from the manufacturer, can be calculated by
- dividing the power consumption by the square of the current: $r = P/I^2$
- Spurious resistance of connections.

Voltage drops in the circuit must be less than the rated operating tolerances of the various loads in steady-state conditions and especially at start-up (inrush current).

Table G.52.1 – Voltage drop

Type of installation	Lighting %	Other uses %
A - Low voltage installations supplied directly from a public low voltage distribution system	3	5
B - Low voltage installation supplied from private LV supply ^a	6	8
* As far as possible, it is recommended that voltage drop within the final installation type A.	al circuits do not exce	ed those indicated in
When the main wiring systems of the installations are longer than 100 n by 0,005 $\%$ per metre of wiring system beyond 100 m, without this supp	n, these voltage drops lement being greater l	may be increased han 0,5 %.
Voltage drop is determined from the demand by the current-using equip	ment, applying diversi	ty factors where



Multipolar low rating use (< 4 A) is not suitable for very-lowvoltage networks (< 24 V DC).

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01-2018 CA908061E





1.1	12/01/2018	Changed title texts	Sonovision
1.0	02/02/2017	Creation	Sonovision
Indice	Date	Modification	Name